

Sub-sized CVN specimen conversion methodology

ASTM A01-13 meeting Tampa 2015
Kim Wallin

ASTM A370 Table 9

TABLE 9 Charpy V-Notch Test Acceptance Criteria for Various Sub-Size Specimens

Full Size, 10 by 10 mm		¾ Size, 10 by 7.5 mm		⅔ Size, 10 by 6.7 mm		½ Size, 10 by 5 mm		⅓ Size, 10 by 3.3 mm		¼ Size, 10 by 2.5 mm	
ft-lbf	[J]	ft-lbf	[J]	ft-lbf	[J]	ft-lbf	[J]	ft-lbf	[J]	ft-lbf	[J]
40 ^A	[54]	30	[41]	27	[37]	20	[27]	13	[18]	10	[14]
35	[48]	26	[35]	23	[31]	18	[24]	12	[16]	9	[12]
30	[41]	22	[30]	20	[27]	15	[20]	10	[14]	8	[11]
25	[34]	19	[26]	17	[23]	12	[16]	8	[11]	6	[8]
20	[27]	15	[20]	13	[18]	10	[14]	7	[10]	5	[7]
16	[22]	12	[16]	11	[15]	8	[11]	5	[7]	4	[5]
15	[20]	11	[15]	10	[14]	8	[11]	5	[7]	4	[5]
13	[18]	10	[14]	9	[12]	6	[8]	4	[5]	3	[4]
12	[16]	9	[12]	8	[11]	6	[8]	4	[5]	3	[4]
10	[14]	8	[11]	7	[10]	5	[7]	3	[4]	2	[3]
7	[10]	5	[7]	5	[7]	4	[5]	2	[3]	2	[3]

^A Table is limited to 40 ft-lbf because the relationship between specimen size and test results has been reported to be non-linear for higher values.

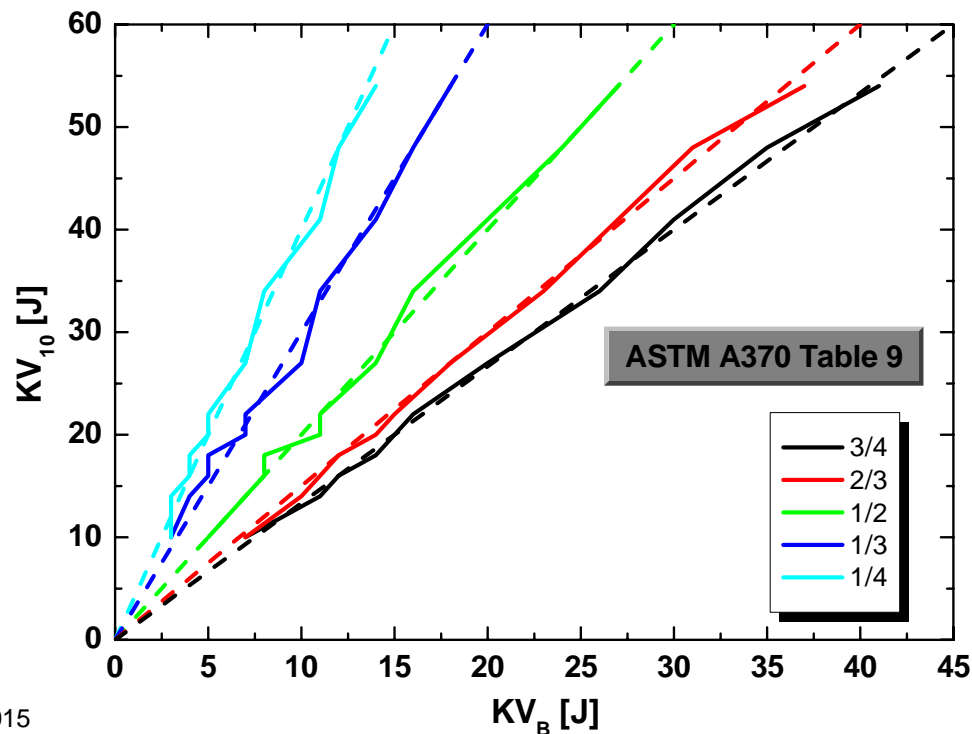
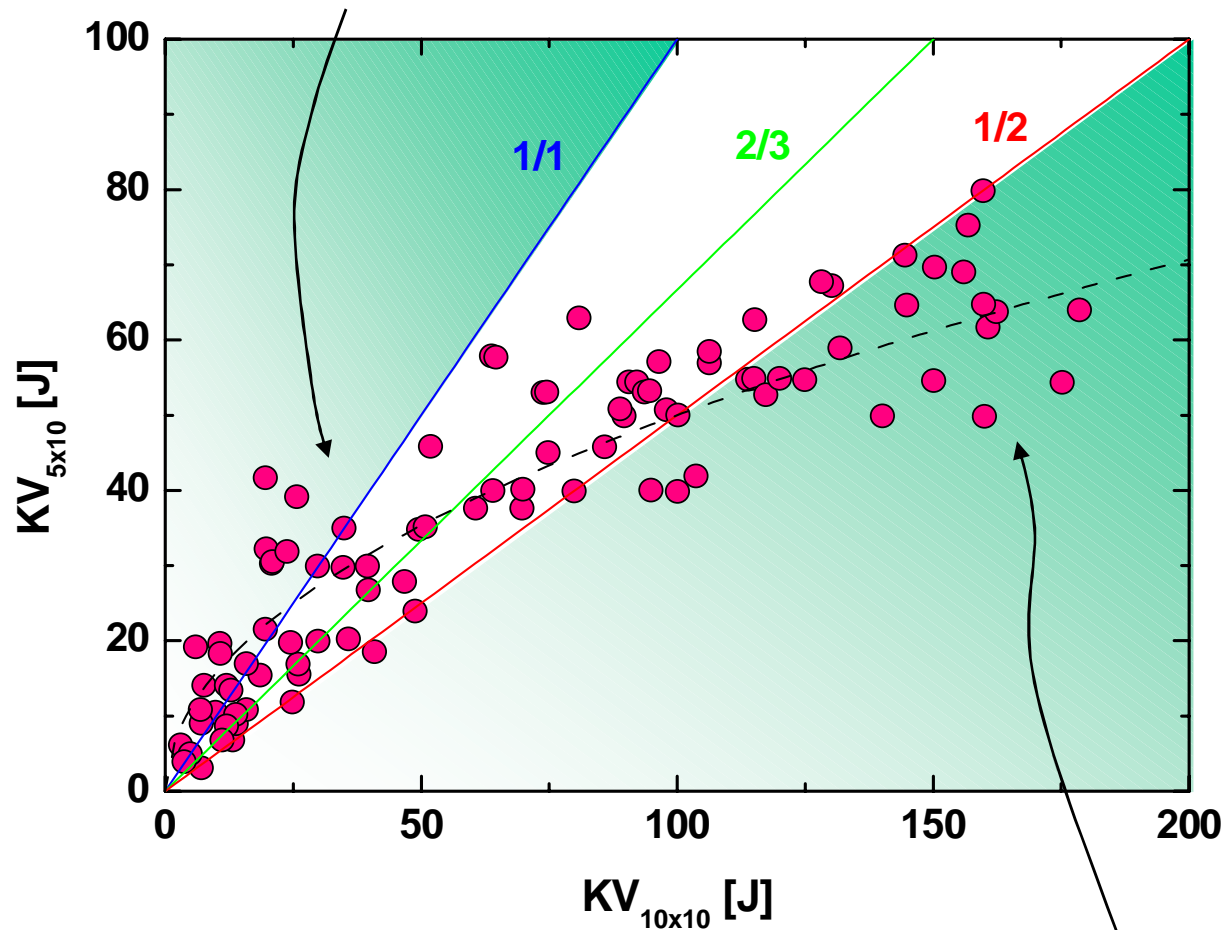


Table 9 is based on a simple thickness-ratio correction.

Subsized specimens

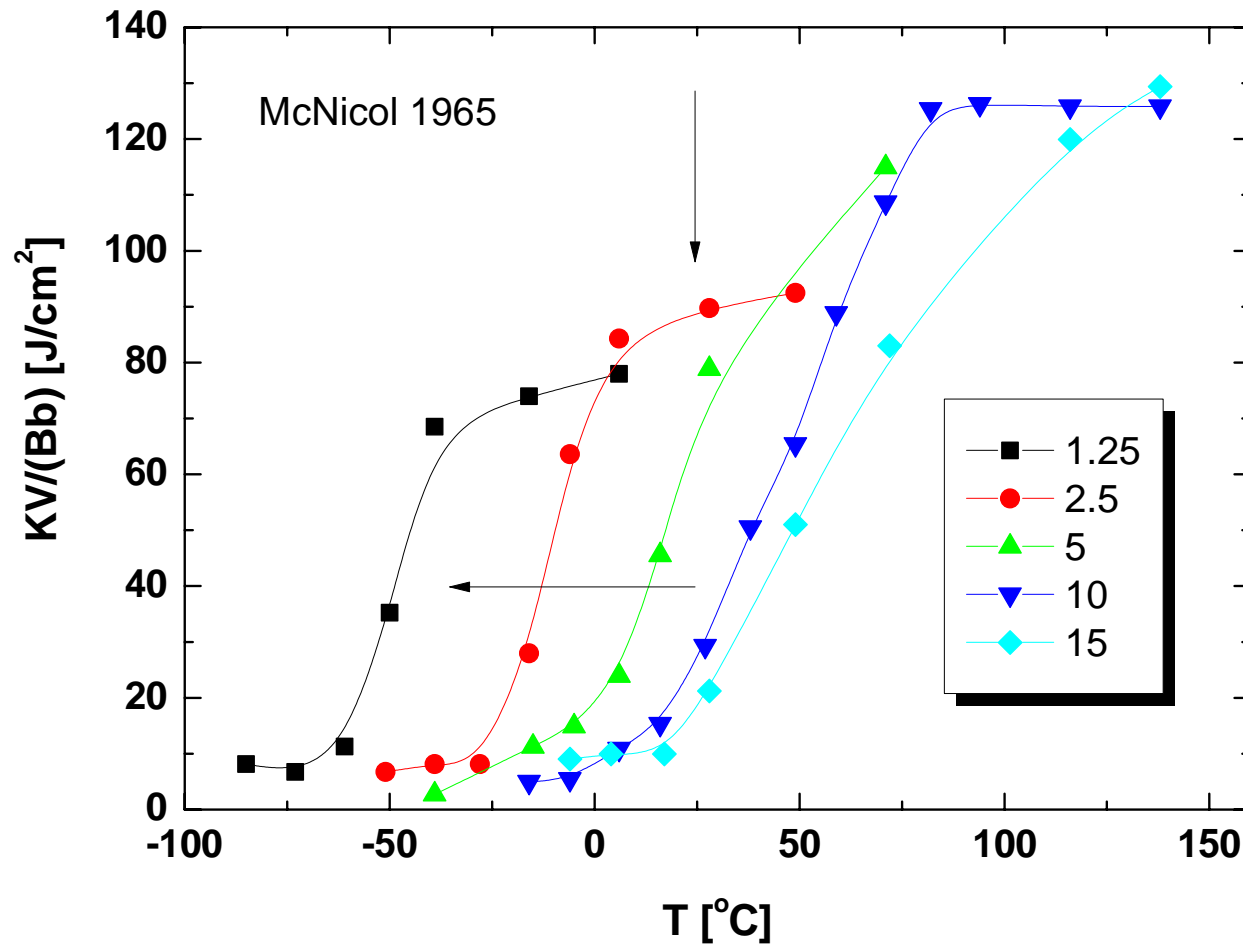
Sub-size specimens yield higher absolute energies



A simple ratio-correction is not sufficient for the adjustment of sub-size Charpy-V specimen energies.

Sub-size specimens yield lower proportional energies

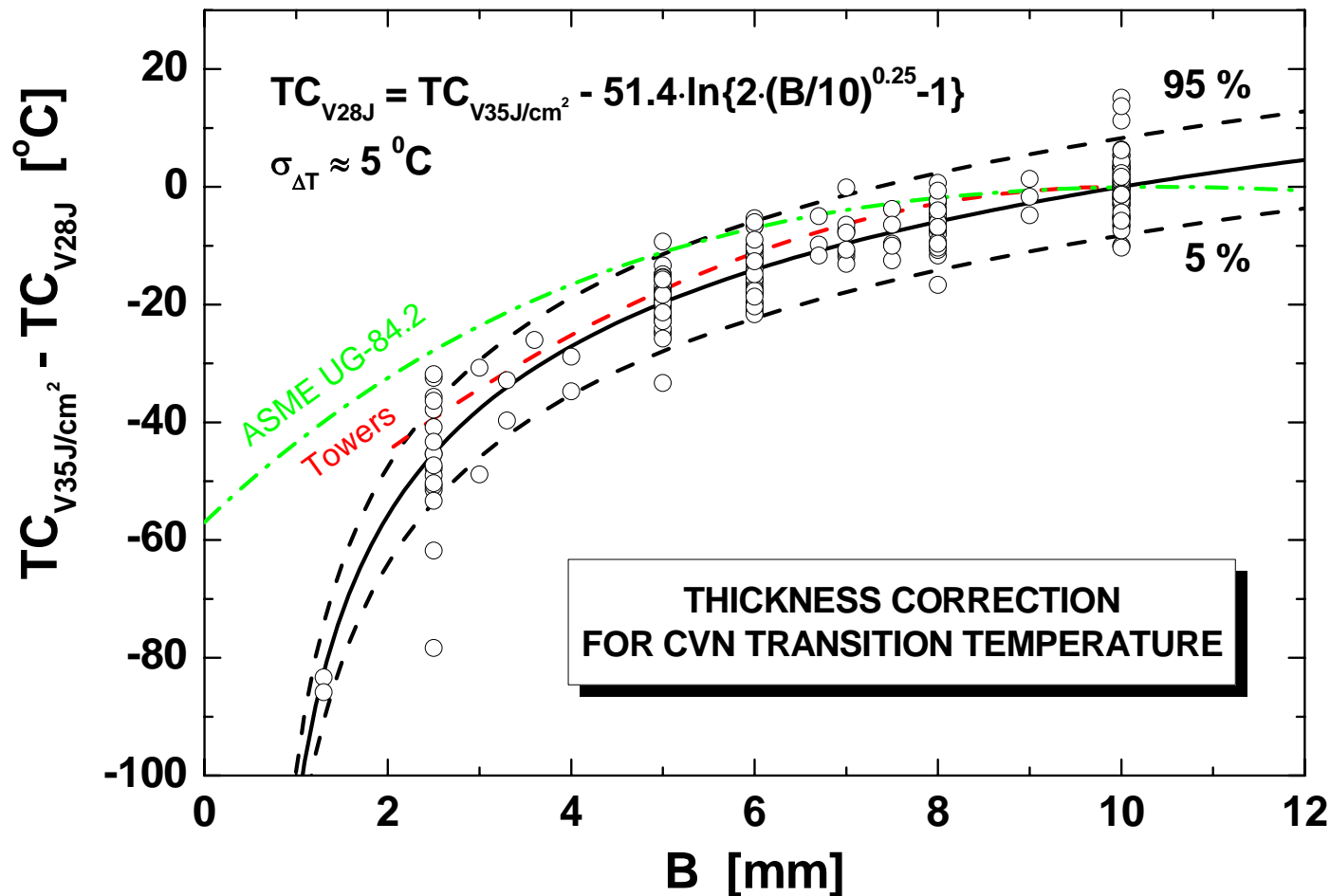
Effect of thickness on transition curve



McNicol, R. (1965, September). Correlation of Charpy Test Results for Standard and Nonstandard Size Specimens. Welding Research Supplement, pp. 385-393.

Subsized specimens

Sub-size specimens yield lower transition temperature

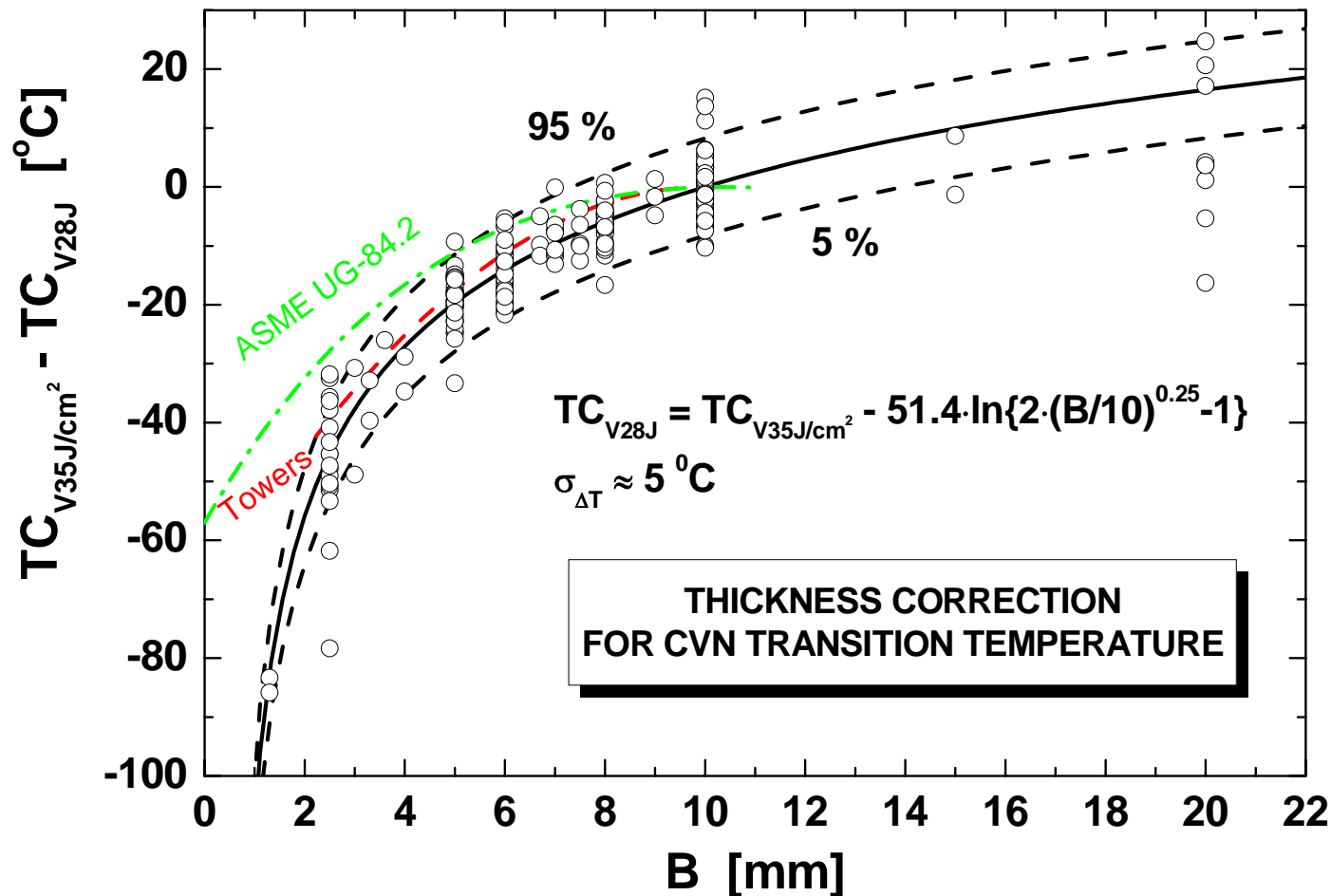


Similar to a statistical size effect related to cleavage initiation. See e.g. ASTM E1921.

**Included in
BS7910-13**

Subsized specimens

Sub-size specimens yield lower transition temperature

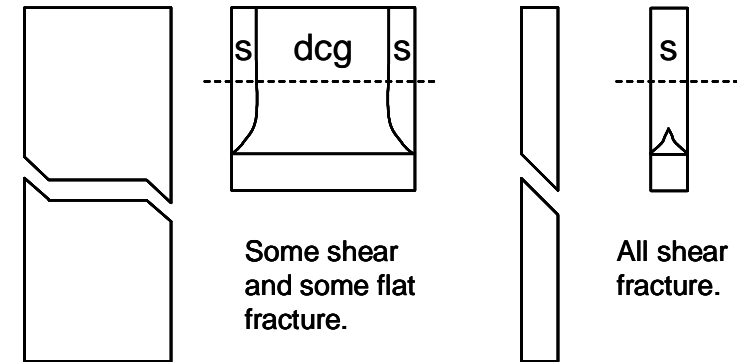
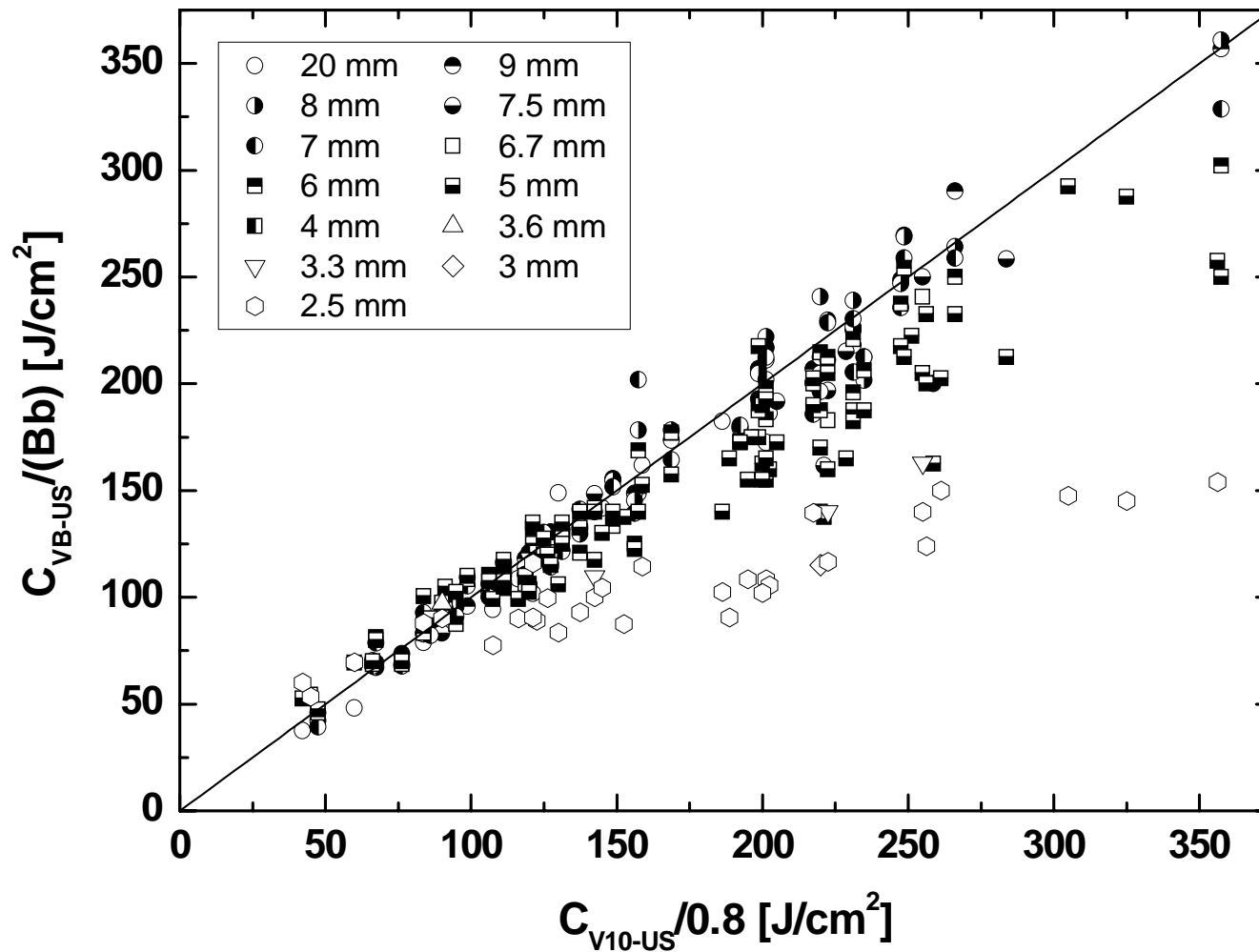


Similar to a statistical size effect related to cleavage initiation. See e.g. ASTM E1921.

**Included in
BS7910-13**

Subsized specimens

Sub-size specimens yield lower proportional upper shelf energies

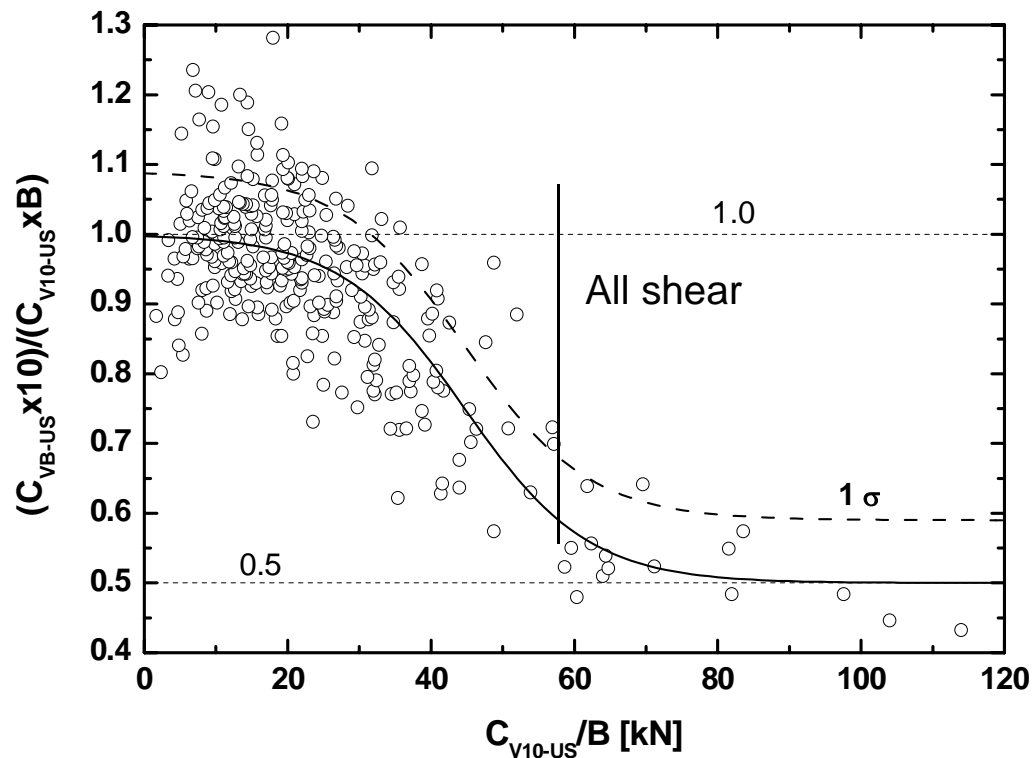


Due to a competition between shear and flat fracture.

Wallin K Upper shelf energy normalisation for sub-sized Charpy-V specimens. Int J of Pressure Vessels and Piping, 78, 2001, pp 463-470.

Subsized specimens

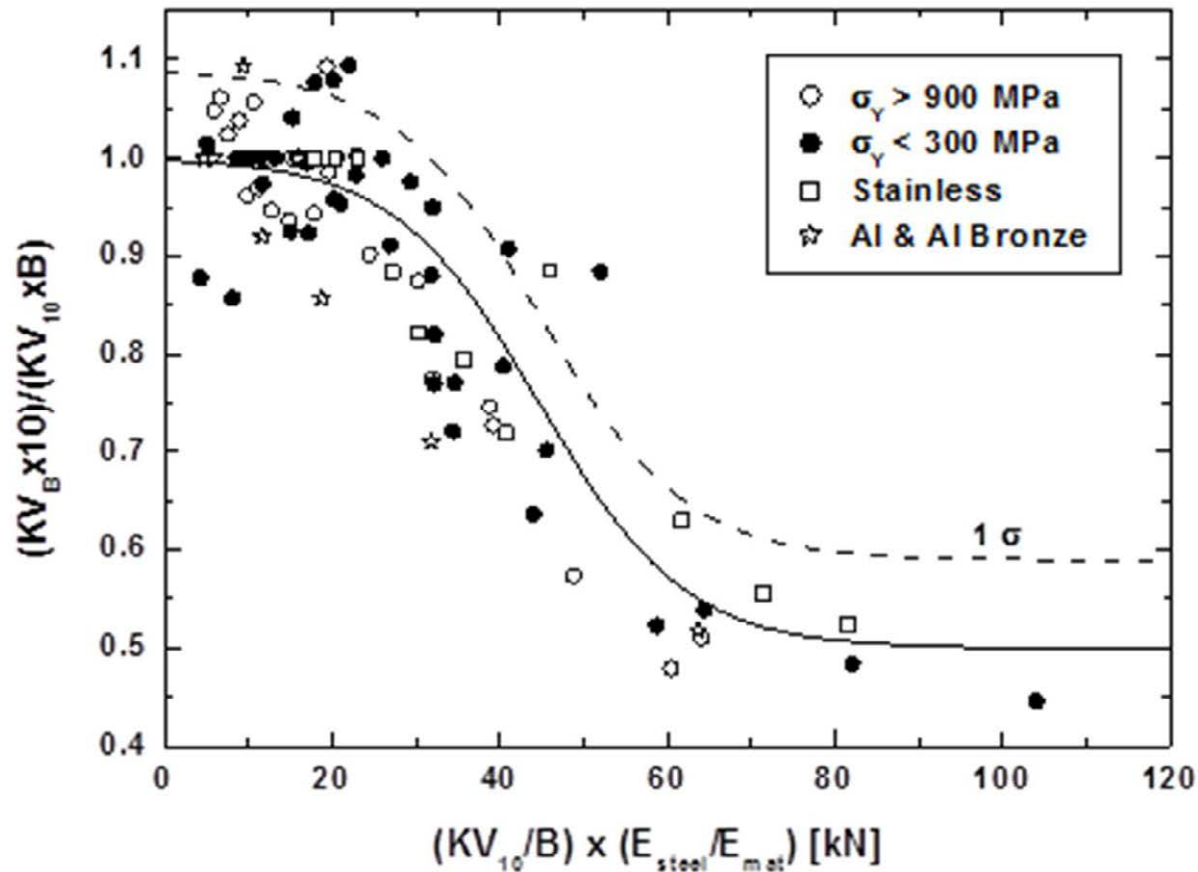
Sub-size specimens yield lower proportional upper shelf energies



$$\frac{C_{VB-US} \cdot 10}{C_{V10-US} \cdot B} = 1 - \frac{0.5 \cdot \exp\left\{\frac{2 \cdot (C_{V10-US} / B - 44.7)}{17.3}\right\}}{1 + \exp\left\{\frac{2 \cdot (C_{V10-US} / B - 44.7)}{17.3}\right\}} \dots [\text{J, mm}]$$

Subsized specimens

Sub-size specimens yield lower proportional upper shelf energies

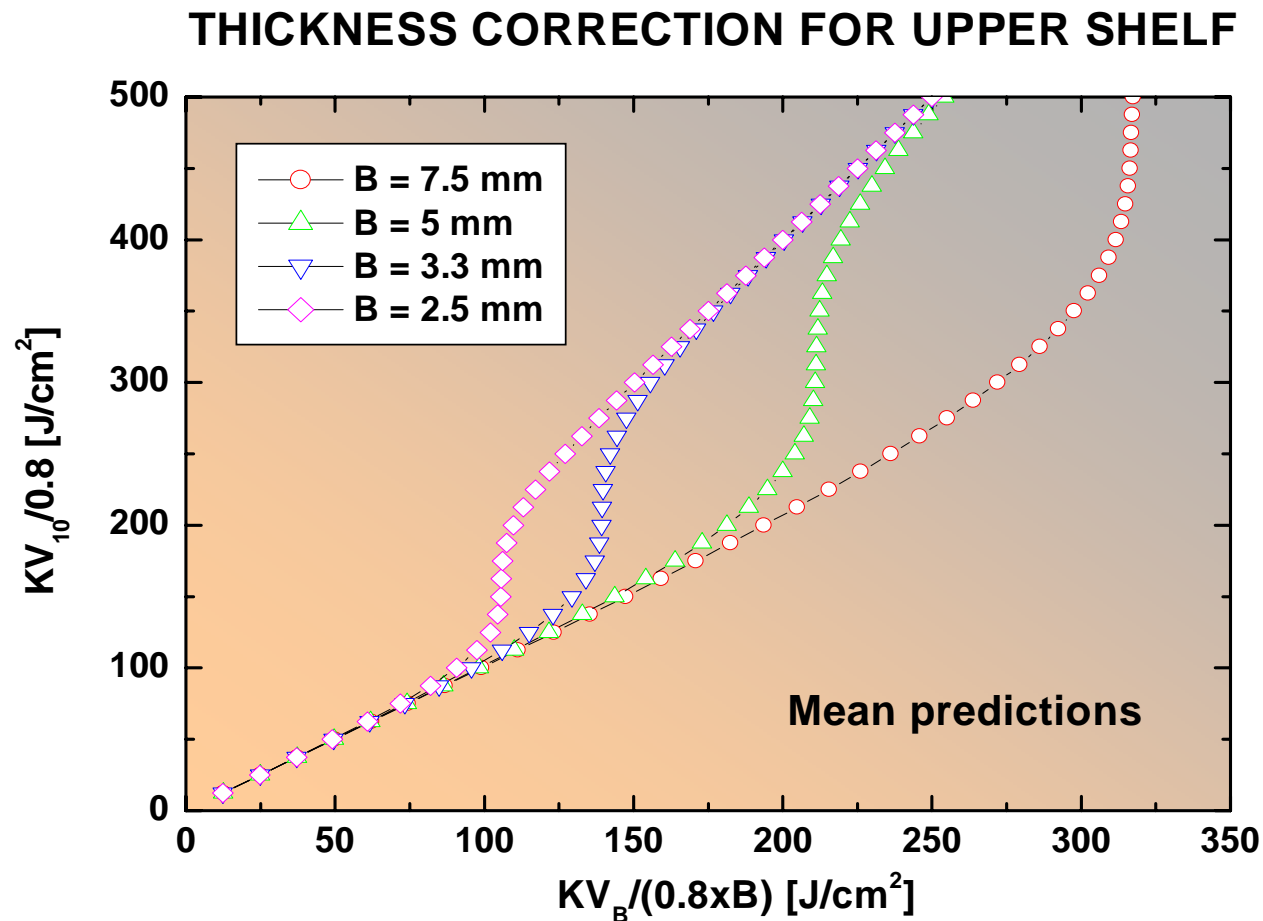


Normalisation is insensitive to strength but sensitive to modulus of elasticity \Rightarrow Austenitic stainless slightly different than structural steel.

Wallin K Upper shelf energy normalisation for sub-sized Charpy-V specimens. Int J of Pressure Vessels and Piping, 78, 2001, pp 463-470.

Subsized specimens

Sub-size specimens yield lower proportional upper shelf energies



Wallin K Upper shelf energy normalisation for sub-sized Charpy-V specimens. Int J of Pressure Vessels and Piping, 78, 2001, pp 463-470.

Temperature adjustment

$$\Delta T = -51.4^{\circ}\text{C} \cdot \ln \left\{ 2 \cdot \left(\frac{B}{10 \text{ mm}} \right)^{0.25} - 1 \right\}$$

Energy conversion

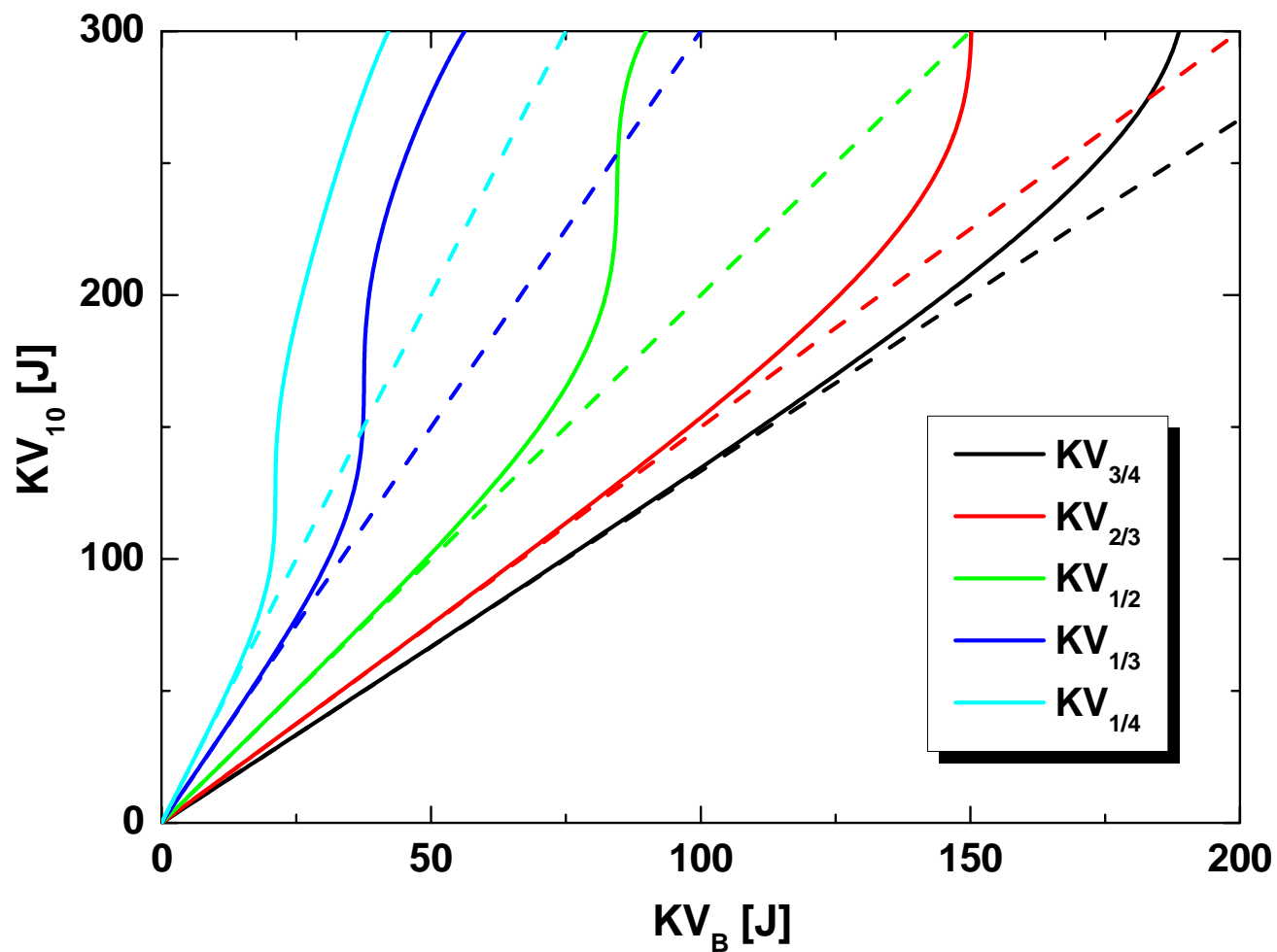
$$\frac{C_{VB} \cdot 10}{C_{V10} \cdot B} \approx 1 - \frac{0.5 \cdot \exp \left\{ \frac{2 \cdot (C_{V10} / B - 44.7)}{17.3} \right\}}{1 + \exp \left\{ \frac{2 \cdot (C_{V10} / B - 44.7)}{17.3} \right\}} \dots [\text{J, mm}]$$

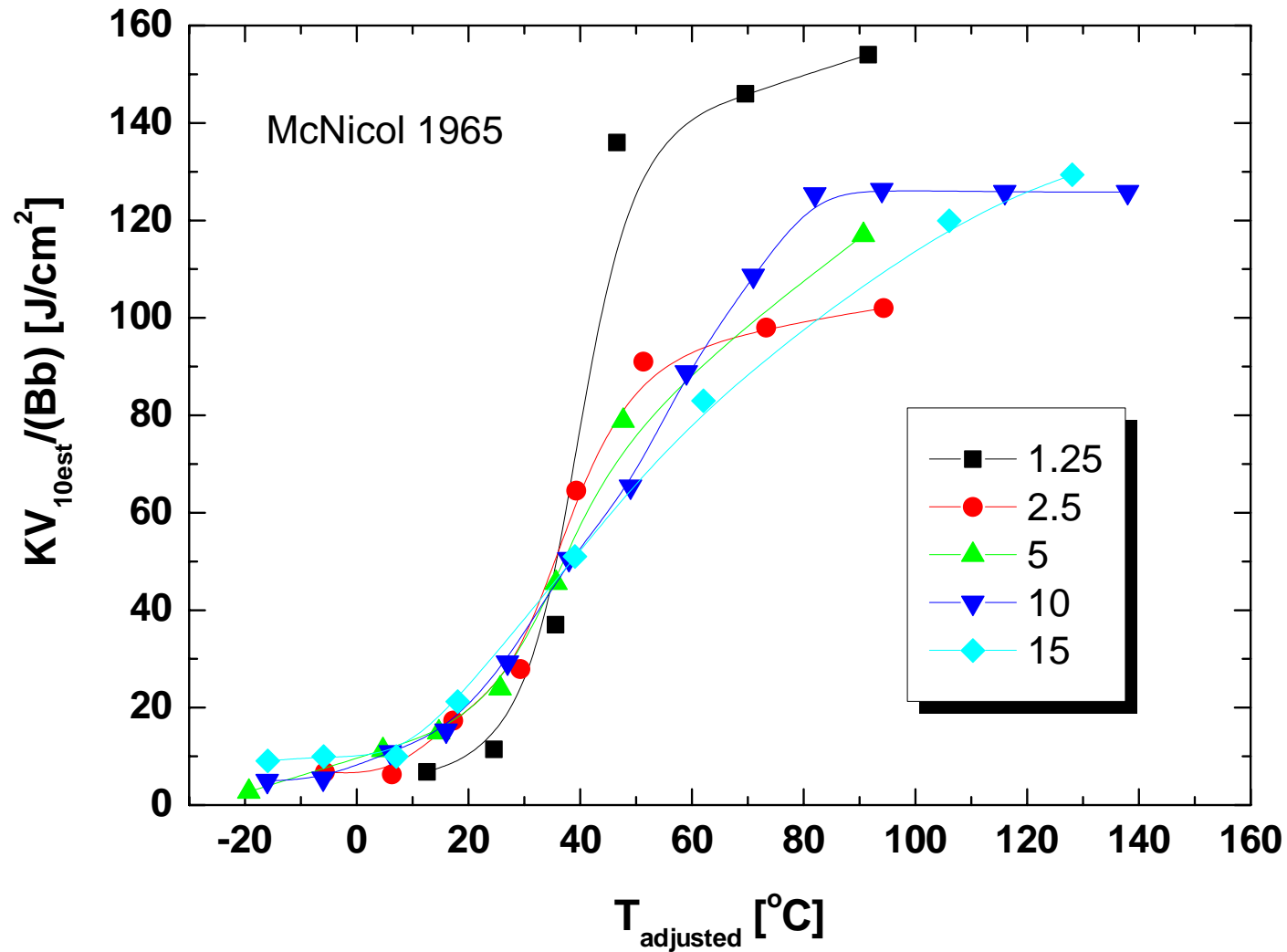
$$\frac{C_{VB-US} \cdot 10}{C_{V10-US} \cdot B} = 1 - \frac{0.5 \cdot \exp\left\{\frac{2 \cdot (C_{V10-US} / B - 44.7)}{17.3}\right\}}{1 + \exp\left\{\frac{2 \cdot (C_{V10-US} / B - 44.7)}{17.3}\right\}} \dots [\text{J, mm}]$$

- The conversion accounts for the lower energy required to fracture shear lips.
- C_{V10-US} corresponds basically to a value without shear lips.
- For high CVN energies the measured full size specimen energy becomes therefore less than indicated by the equation.
- Begins to effect when $C_{V10} > 100 \text{ J}$.

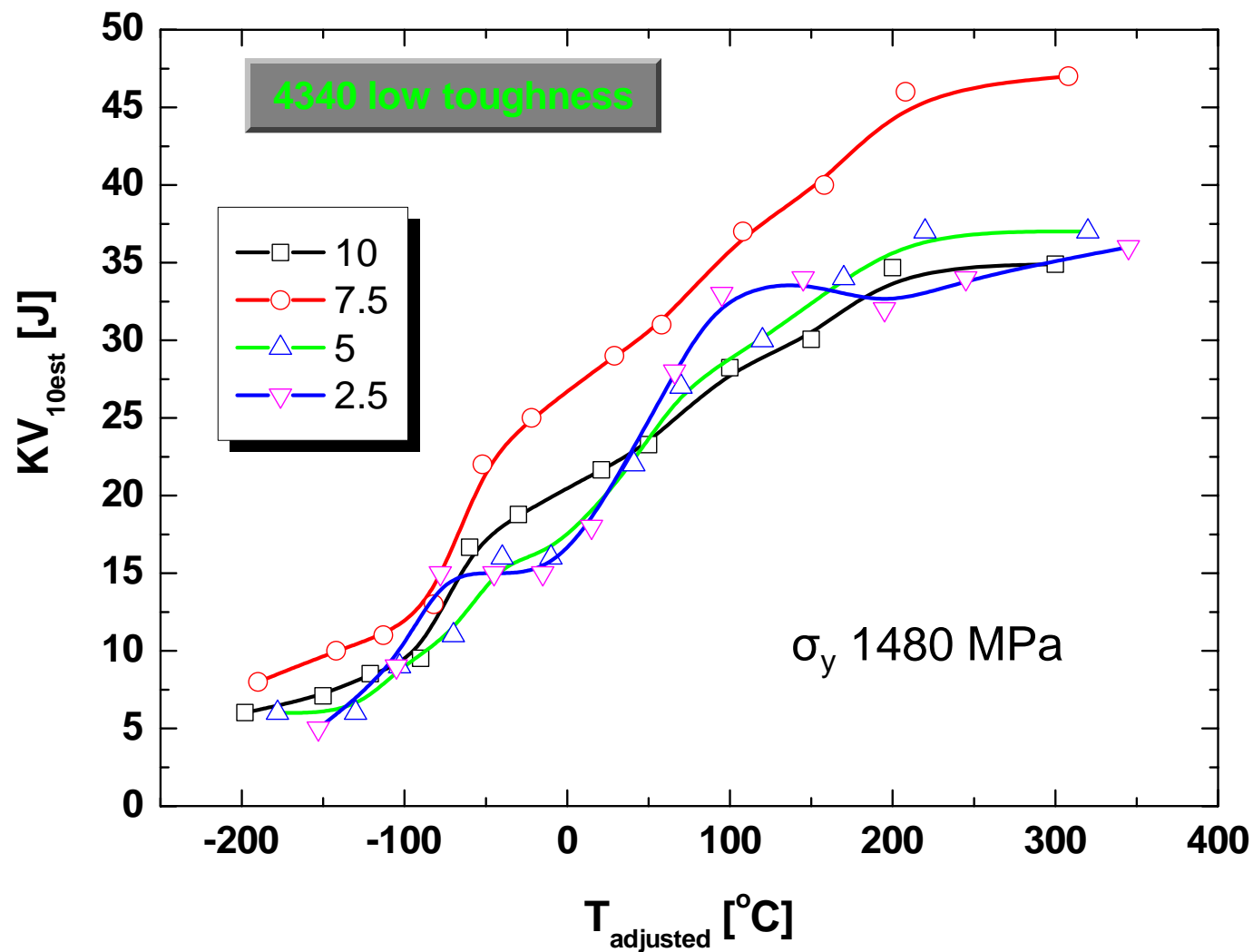
Energy conversion

Estimated
measured
energy.

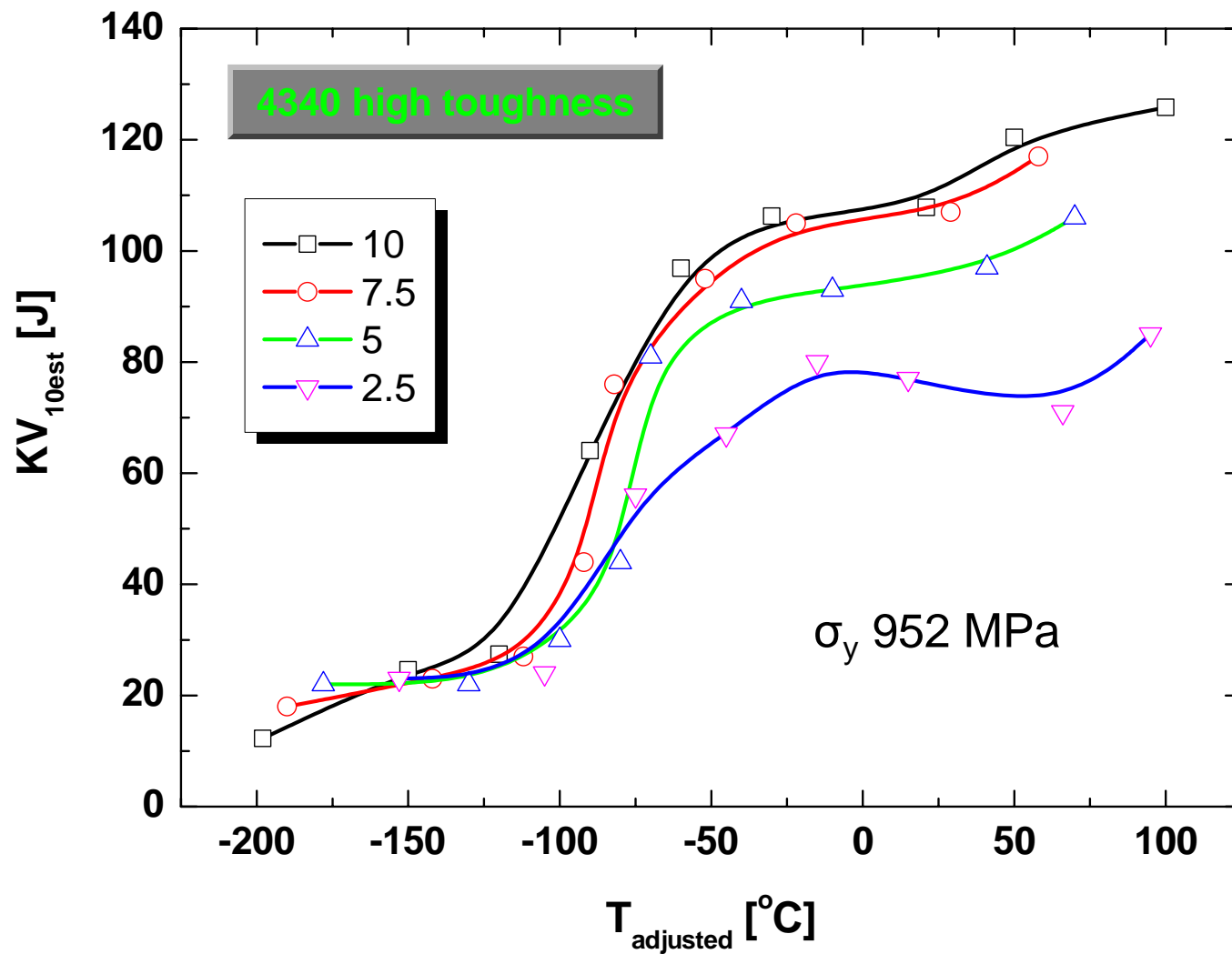




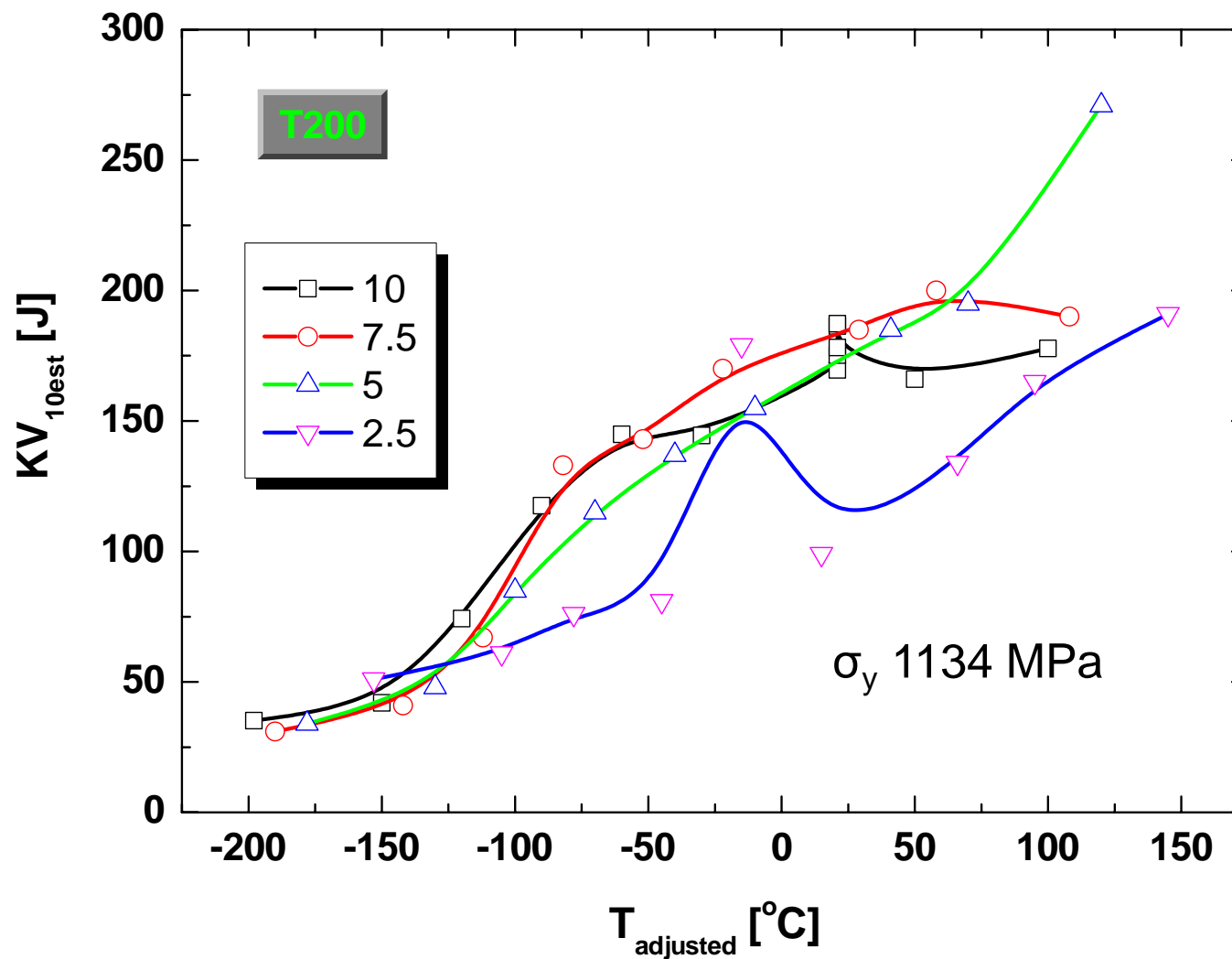
McNicol, R. (1965, September). Correlation of Charpy Test Results for Standard and Nonstandard Size Specimens. Welding Research Supplement, pp. 385-393.



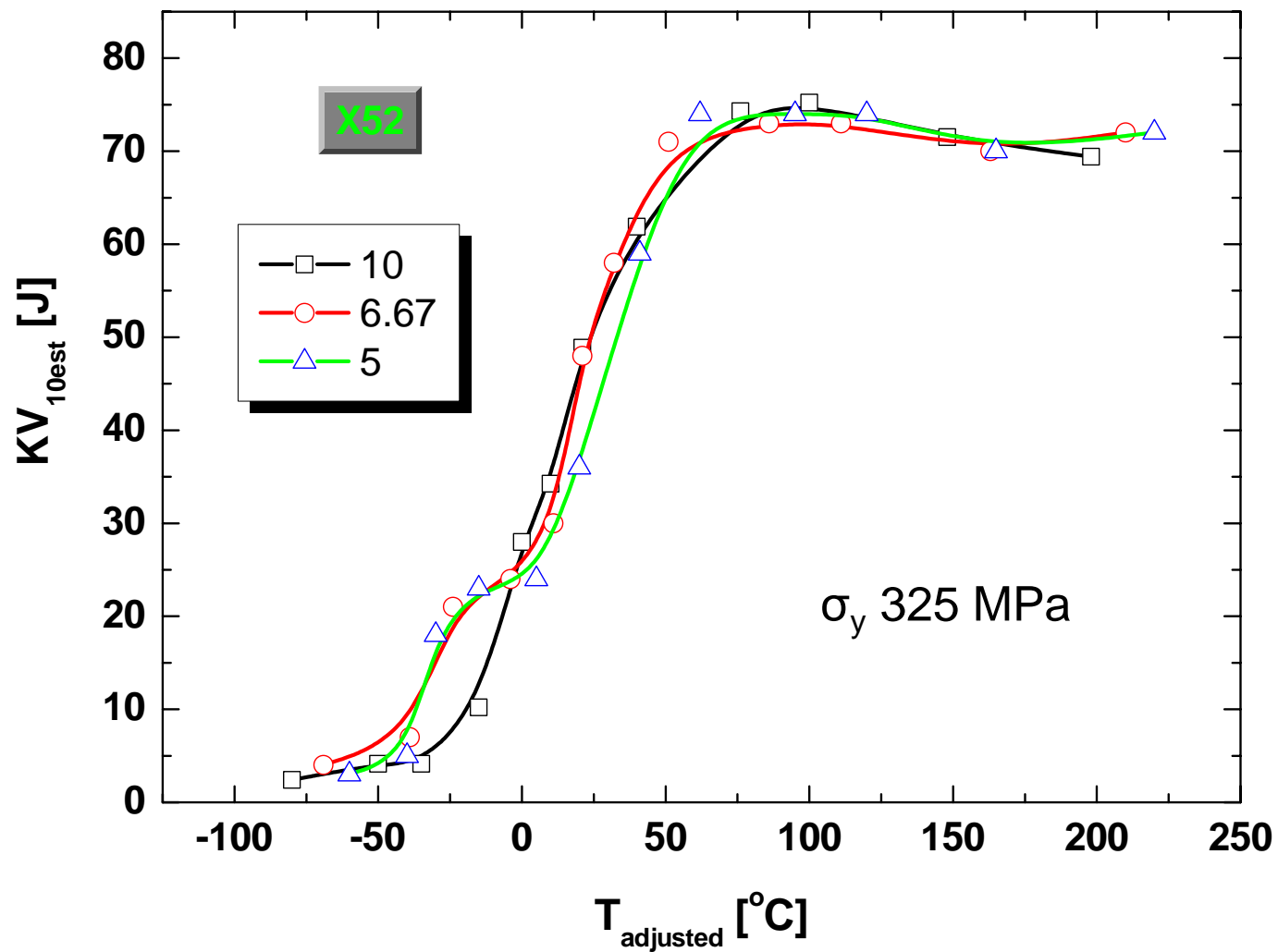
Enrico Lucon, C. N. (2015). Impact Characterization of 4340 and T200 Steels by Means of Standard, Sub-Size and Miniaturized Charpy Specimens. NIST Technical Note 1858.



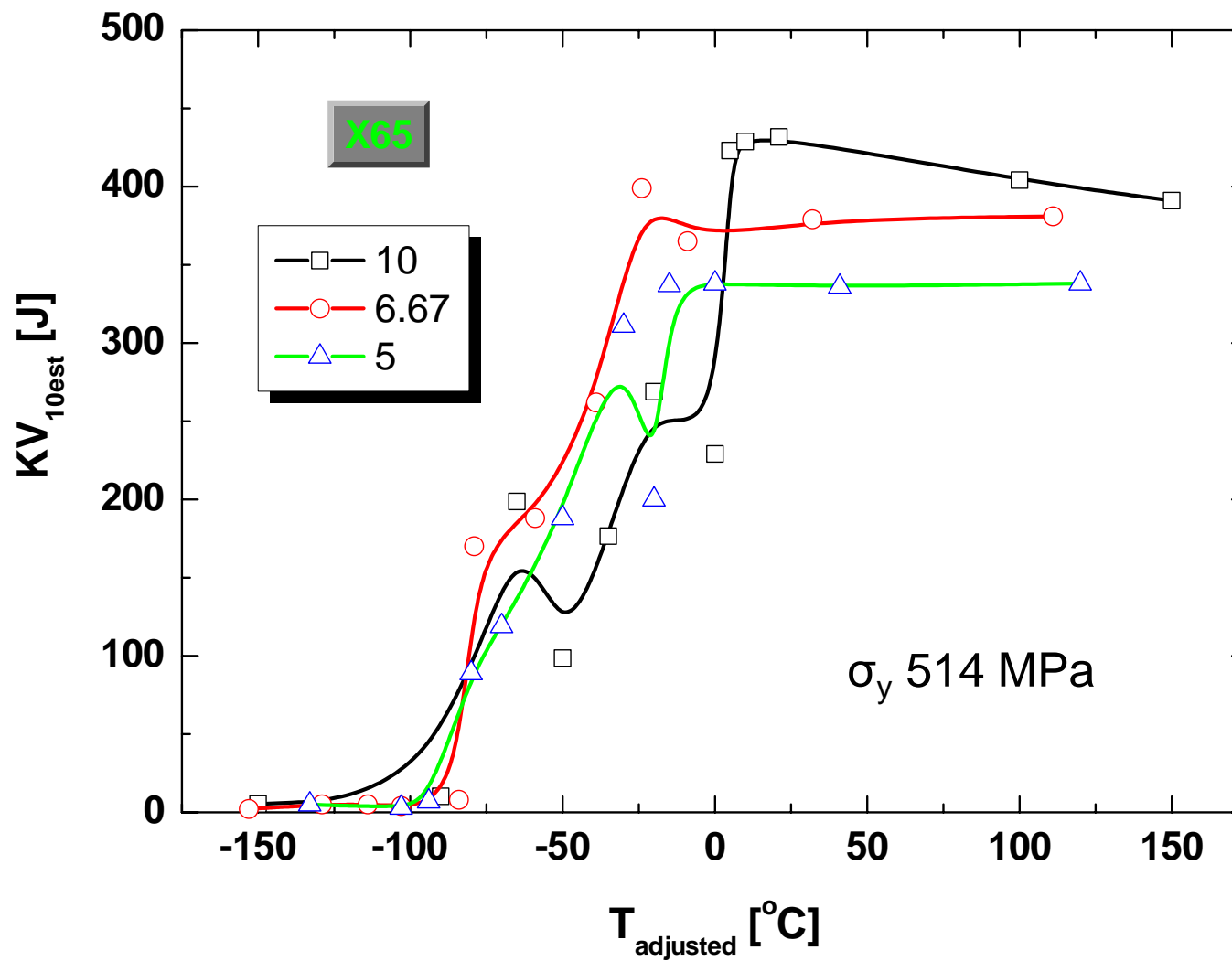
Enrico Lucon, C. N. (2015). Impact Characterization of 4340 and T200 Steels by Means of Standard, Sub-Size and Miniaturized Charpy Specimens. NIST Technical Note 1858.



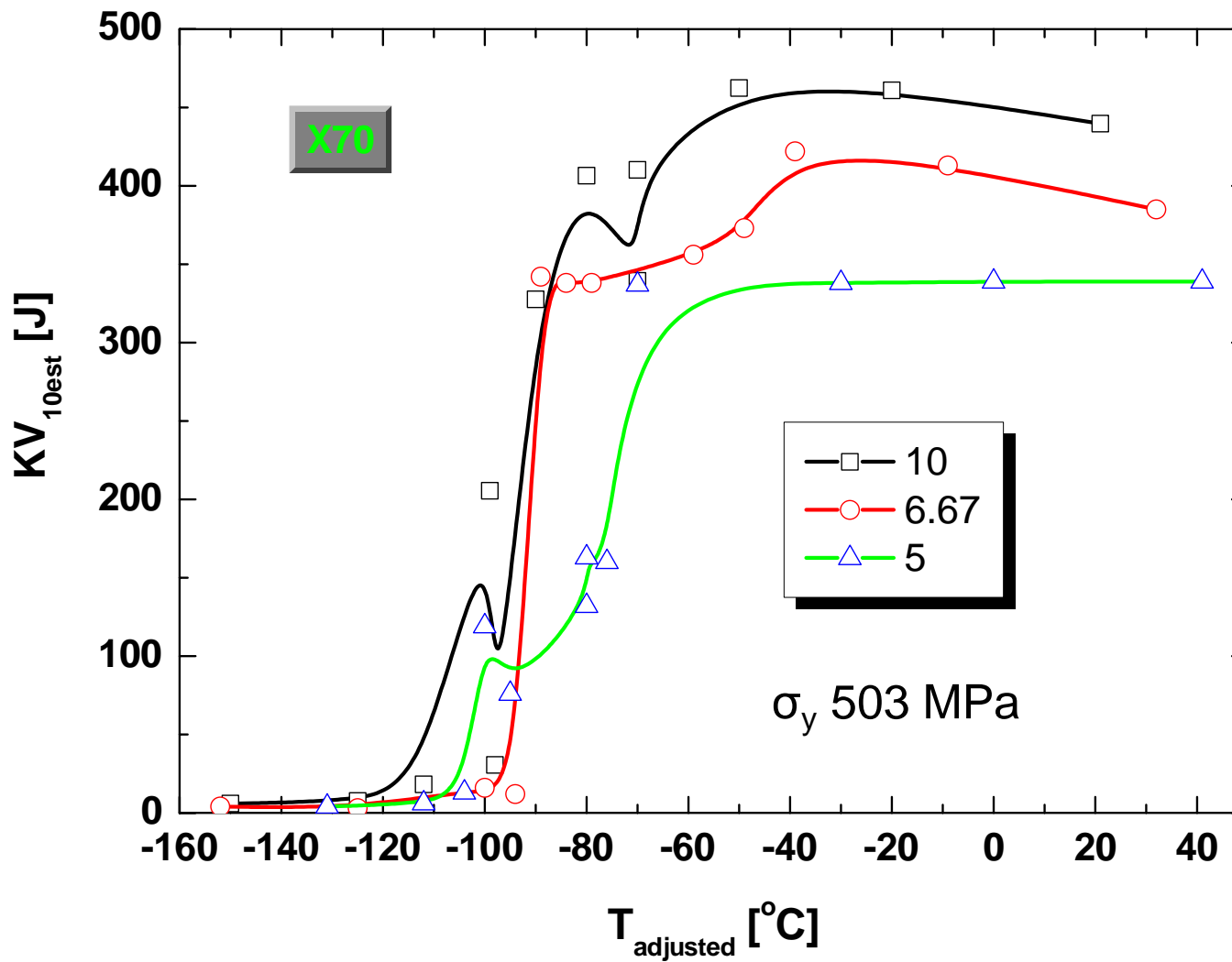
Enrico Lucon, C. N. (2015). Impact Characterization of 4340 and T200 Steels by Means of Standard, Sub-Size and Miniaturized Charpy Specimens. NIST Technical Note 1858.



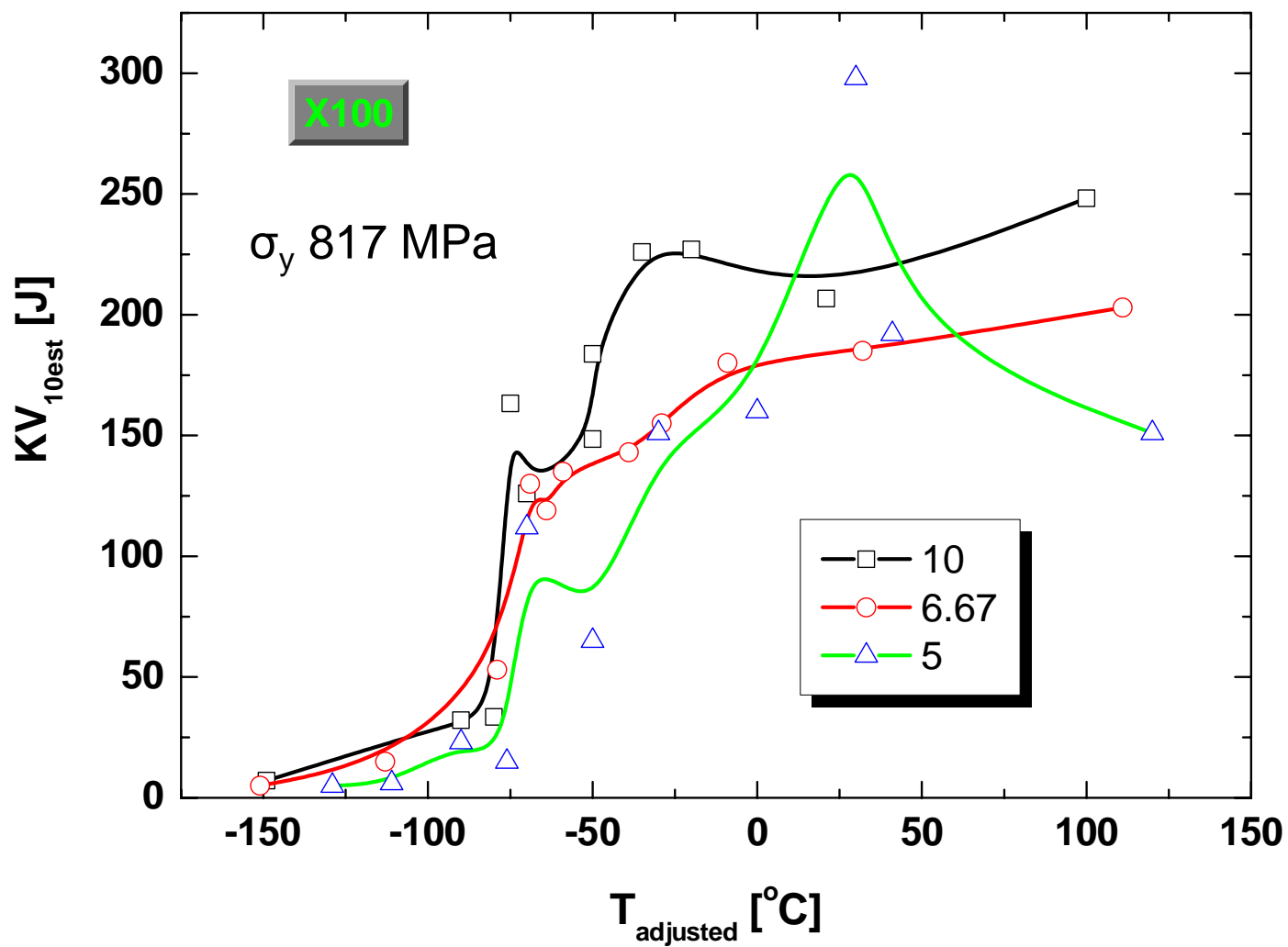
E. Lucon, C. N. McCowan, and R. L. Santoyo, (2015). Impact Characterization of Line Pipe Steels by Means of Standard, Sub-Size and Miniaturized Charpy Specimens. NIST Technical Note 1865.



E. Lucon, C. N. McCowan, and R. L. Santoyo, (2015). Impact Characterization of Line Pipe Steels by Means of Standard, Sub-Size and Miniaturized Charpy Specimens. NIST Technical Note 1865.

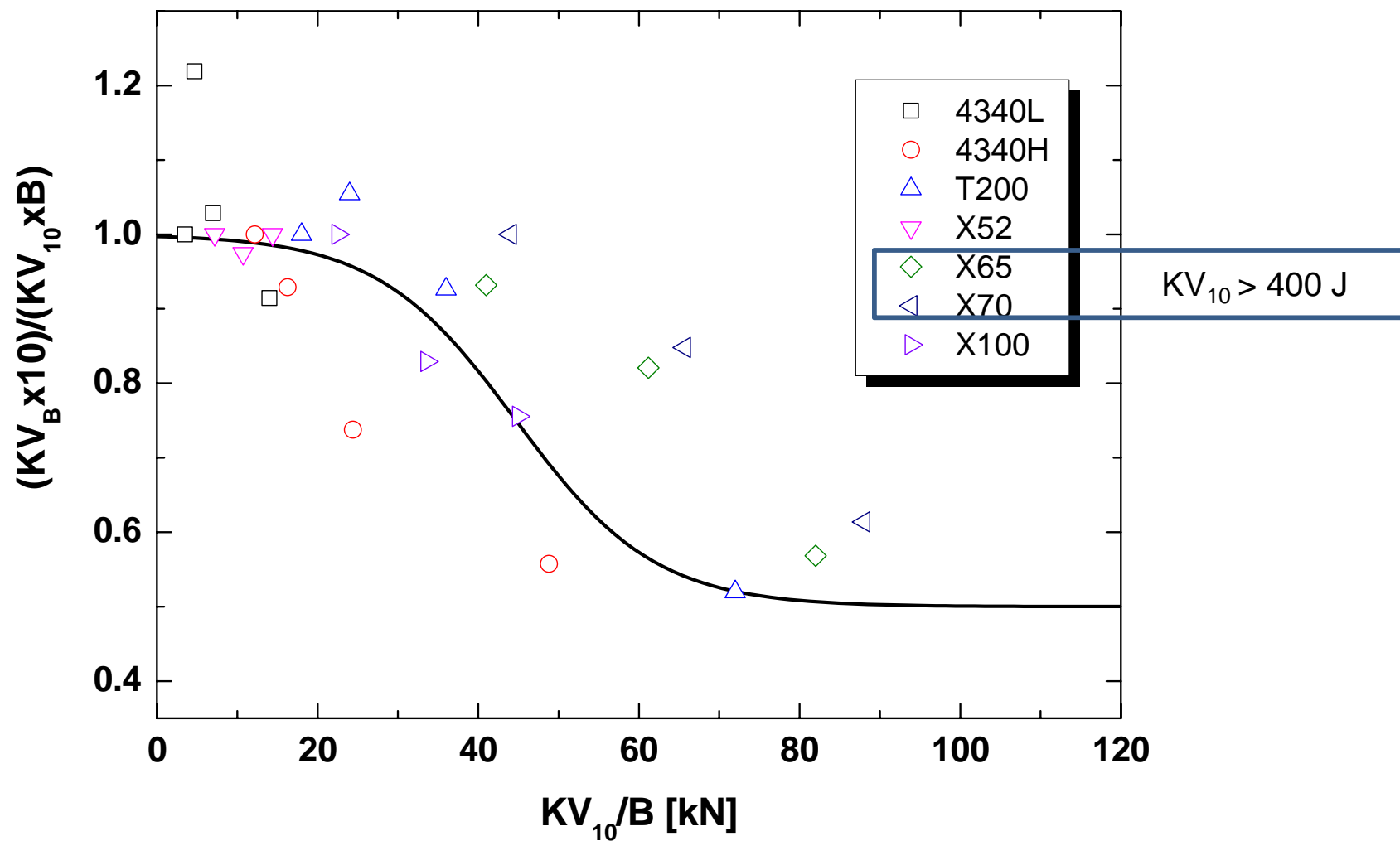


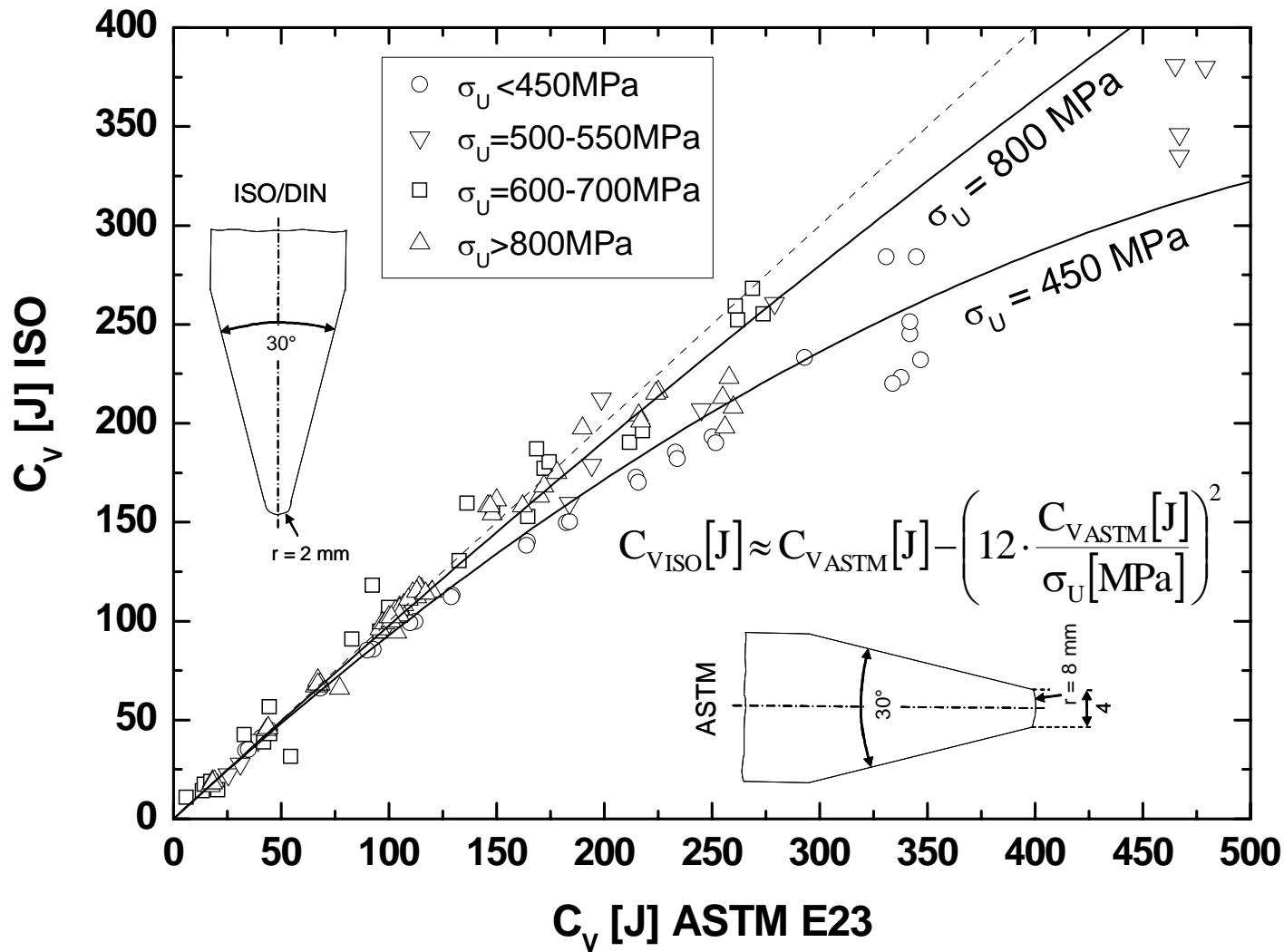
E. Lucon, C. N. McCowan, and R. L. Santoyo, (2015). Impact Characterization of Line Pipe Steels by Means of Standard, Sub-Size and Miniaturized Charpy Specimens. NIST Technical Note 1865.



E. Lucon, C. N. McCowan, and R. L. Santoyo, (2015). Impact Characterization of Line Pipe Steels by Means of Standard, Sub-Size and Miniaturized Charpy Specimens. NIST Technical Note 1865.

Upper shelf behaviour





The ASTM hammer show for high toughness higher energies than the ISO hammer

energy conversion

Full size [J]	3/4 [J]	2/3 [J]	1/2 [J]	1/3 [J]	1/4 [J]
10	7	7	5	3	2
14	10	9	7	5	3
16	12	11	8	5	4
18	13	12	9	6	4
20	15	13	10	7	5
22	16	15	11	7	5
27	20	18	13	9	7
34	25	23	17	11	8
41	31	27	20	14	10
48	36	32	24	16	12
54	40	36	27	18	13
60	45	40	30	20	14
68	51	45	34	22	16
76	57	51	38	25	18
86	65	57	43	27	19
100	75	66	49	31	20

temperature adjustment

Thickness	Adjustment [°C]
Full size	0
3/4	8
2/3	11
1/2	20
1/3	34
1/4	45



TECHNOLOGY «» FOR BUSINESS

